



ECE 344

Microwave Fundamentals

Assistant Professor
Dr. Gehan Sami

lect4

Ideal transmission line component in ADS

Example 1

Figure shows an ideal transmission line in the ADS schematic window. The **E** in the figure represents the electrical length



TLIN

TL1

Z=50.0 Ohm

E=90

F=1 GHz

Figure An ideal transmission line component in ADS

- (1) If the wavelength at 1 GHz is denoted as λ_0 , what is the length of the transmission line?
- (2) What is the electrical length **E** at a frequency of 3 GHz?

Solutions

- (1) Since

$$\theta = \beta l = \frac{2\pi l}{\lambda_0} = \frac{\pi}{2}$$

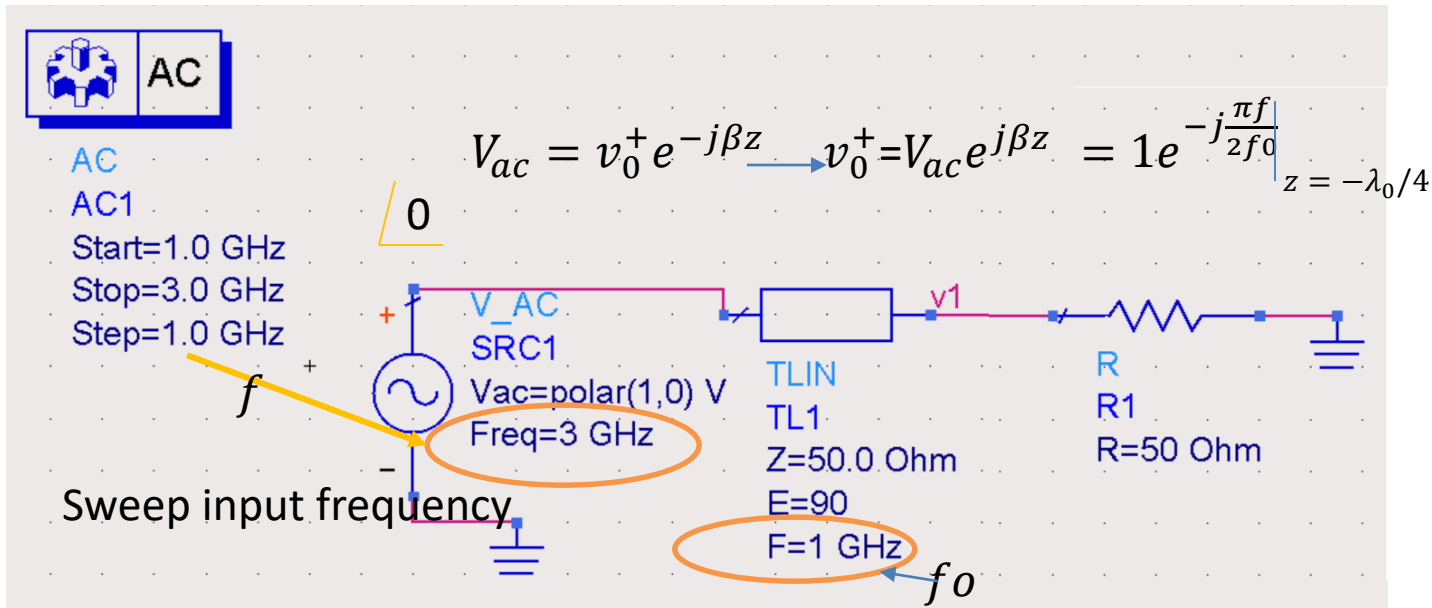
then the length is found to be $l = 0.25 \lambda_0$. physical length if fabricated=7.5 cm

- (2) The electrical length is

$$\theta = \beta l = \frac{\omega l}{v_p} = \frac{2\pi l}{\lambda}$$

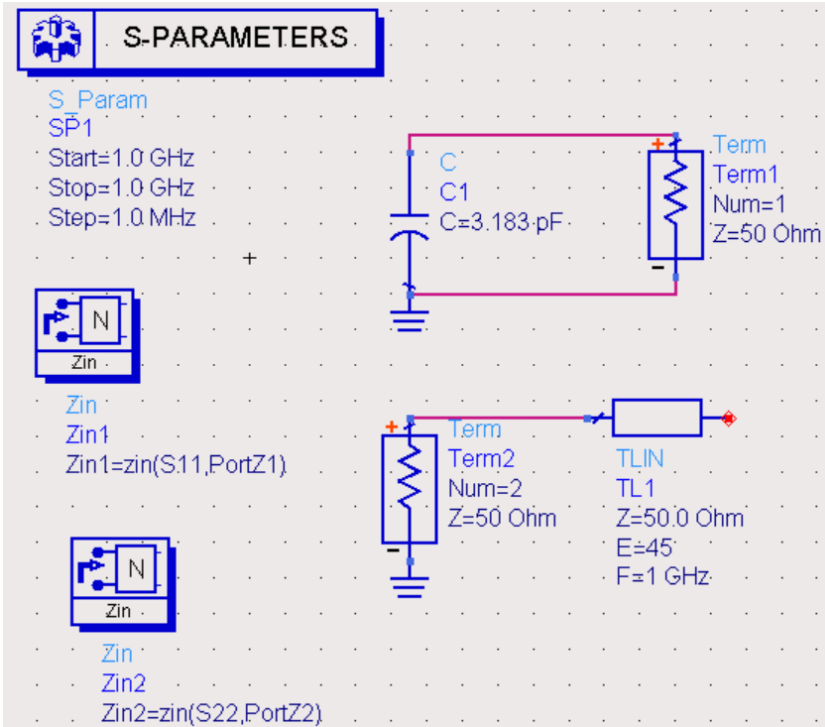
Now, keeping the phase velocity and length fixed, the electrical length is proportional to the frequency. Thus, at 3 GHz, $|\mathbf{E}| = 270^\circ$.

Verify by ADS



freq	v1
1.000 GHz	1.000 / -90.000
2.000 GHz	1.000 / -179.999
3.000 GHz	1.000 / 90.000

Example 2 Open end and short end TL equivalent elements

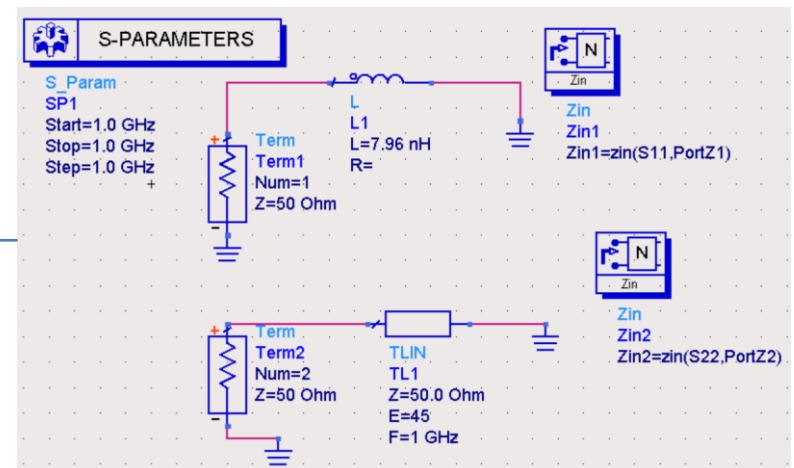


freq	Zin1	Zin2
1.000 GHz	50.002 / -90.000	50.000 / -90.000

openTLequivC

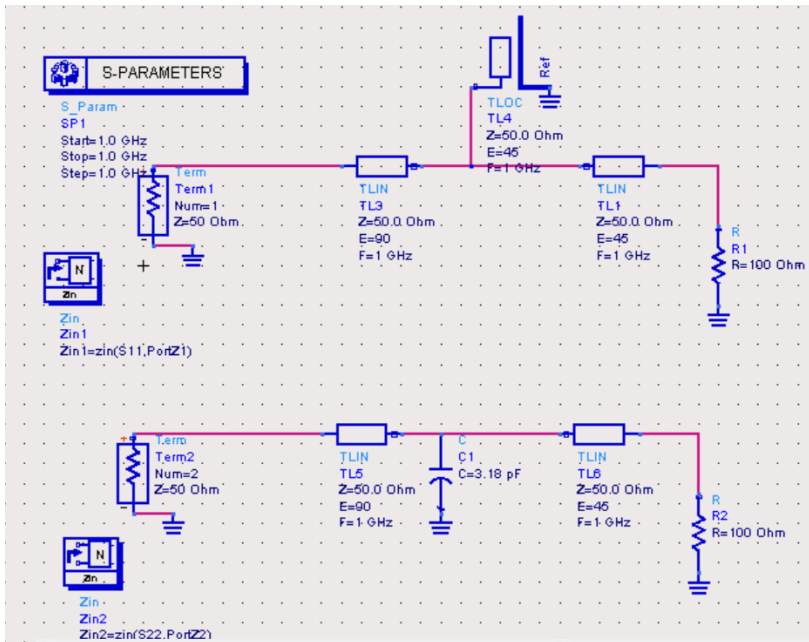
shortTLequivL

freq	Zin1	Zin2
1.000 GHz	50.014 / 90.000	50.000 / 90.000



Example 3

Zin for microwave circuit contain $\lambda/8$ open end TL and its equivalent capacitor (OC TL is shunt connection as its equivalent capacitor), using schematic and smith-chart utility



freq	Zin1	S(1,1)	Zin2	S(2,2)
1.000 GHz	40.000 + j80.000	0.670 / 55.491	40.000 + j79.951	0.669 / 55.513

Gamma: 0.66953 < 55.4915 Z: 40.0000 +j 80.0000

VSWR: 5.05206 Y: 0.00500 +j -0.01000

Network Schematic

Delete Selected Component Set Defaults...

Zo: 50.0 Value: 90.000 Deg Loss: 3.000 dB/m

Example 4

A 50Ω line of length $\lambda/2$ is connected at one end to a reflectionless 50Ω generator. The other end is terminated alternatively with load $Z = Z_1$, or $Z = Z_2$.

Determine for the two terminations $Z = Z_1$, $Z = Z_2$.

- The reflection coefficient of the load Γ
- The input impedance on the generator side Z'

Where $Z_1 = 50\Omega$, and $Z_2 = 30 - j40\Omega$

Solution: At length $\lambda/2$ $\tan\beta l = 0$ and $Z_{in} = Z_L$

At Z_1 $\Gamma = 0$, $Z_{in} = Z_1$

At Z_2 $\Gamma = -j0.5$ $Z_{in} = Z_2$

Use smithchart utility to check your answer:

For Z_2

Network Schematic

Define Source/Load Network Terminations...

Freq (GHz): 1 Z0 (Ohms): 50 Normalize

Network Schematic

Diagram showing a source impedance Z_S^* connected to a load impedance Z_L .

Value: $30-j*40$

Gamma: 0.50000 Z: 30.0000 +j -40.0000

VSWR: 3.00000 Y: 0.01200 +j 0.01600

Example 5

Given a 50Ω transmission line that is 0.25λ long excited by a 1 V voltage source at 300 MHz frequency with an internal impedance of 100Ω , and the line is terminated by a load

$Z_L = 100 - j40 \Omega$, determine $\Gamma_L, Z_{in}, V_{in}, V_o^+$

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o} = 0.378 - j0.166$$

$$Z_{in} = Z_o * Z_o / Z_L = 21.55 + j8.62$$

$$V_{in} = V_{TH} \frac{Z_{in}}{Z_{in} + Z_{TH}} = 0.1814 + j0.058$$

$$V_o^+ = \frac{V_{in}}{e^{j\beta l} (1 + \Gamma_L e^{-2j\beta l})} = 0.0144 - j0.295$$

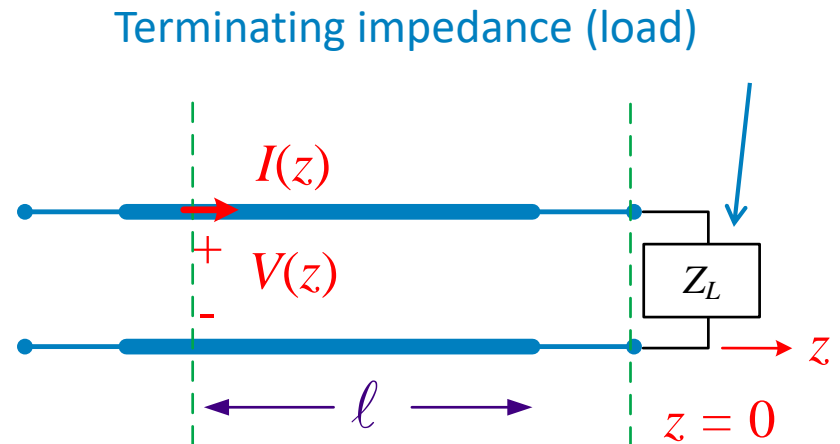
Terminated Transmission Line (cont.)

$$V(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z}$$

What if we know

V^+ and V^- @ $z = -\ell$

Can we use $z = -\ell$ as a reference plane?



$$V_0^+ = V^+(0) = V^+(-\ell) e^{-\gamma \ell}$$

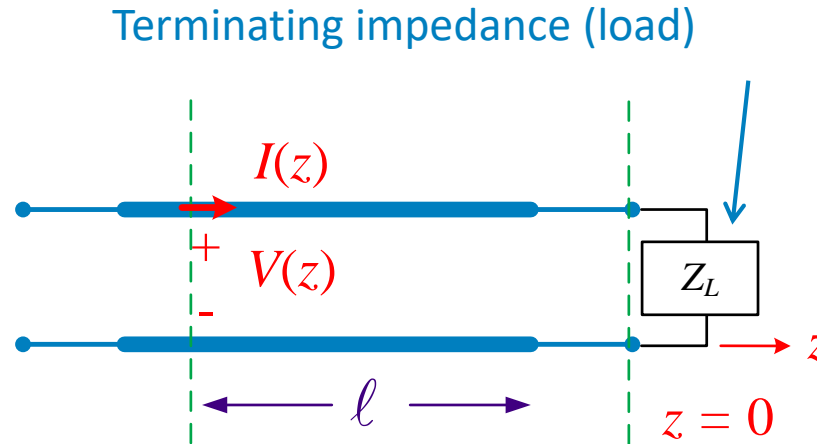
$$V^-(-\ell) = V^-(0) e^{-\gamma \ell}$$

$$\Rightarrow V_0^- = V^-(0) = V^-(-\ell) e^{\gamma \ell}$$

Hence

$$V(z) = V^+(-\ell) e^{-\gamma(z+\ell)} + V^-(-\ell) e^{\gamma(z+\ell)}$$

Terminated Transmission Line (cont.)



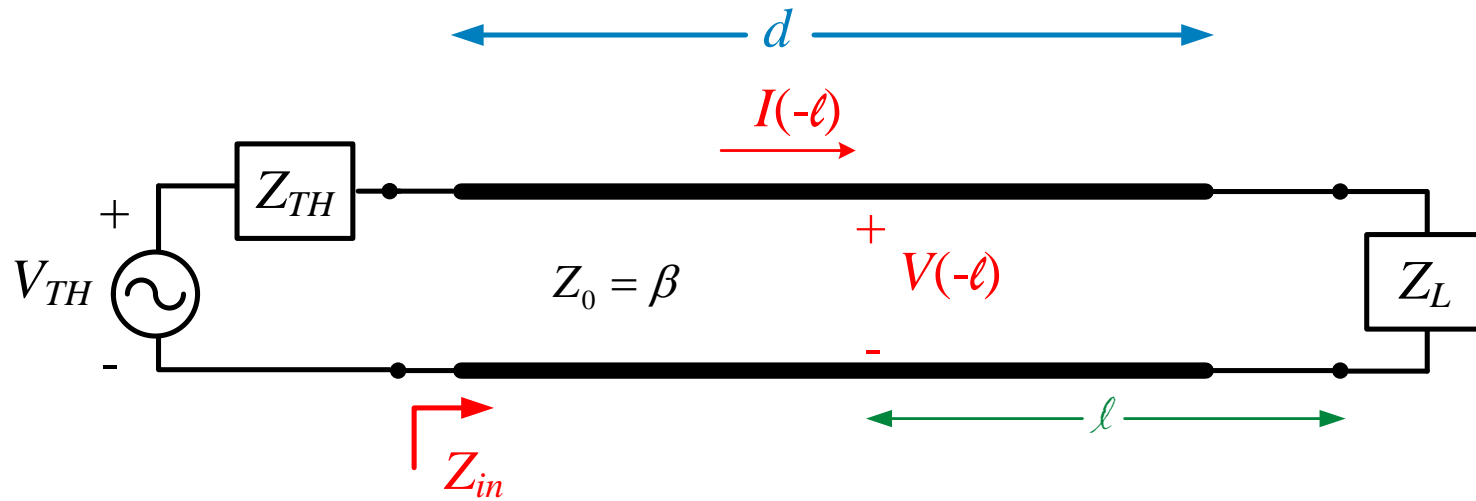
Compare:

$$V(z) = V^+(0)e^{-\gamma z} + V^-(0)e^{+\gamma z}$$

$$V(z) = V^+(-\ell)e^{-\gamma(z-(-\ell))} + V^-(-\ell)e^{\gamma(z-(-\ell))}$$

Note: This is simply a change of reference plane, from $z = 0$ to $z = -\ell$.

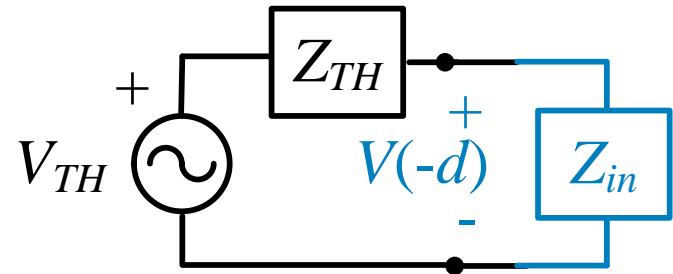
Example



Find the voltage at any point on the line.

$$Z_{in} = Z(-d) = Z_0 \left(\frac{Z_L + jZ_0 \tan(\beta d)}{Z_0 + jZ_L \tan(\beta d)} \right)$$

$$\Rightarrow V(-d) = V_{TH} \left(\frac{Z_{in}}{Z_{in} + Z_{TH}} \right)$$



Example (cont.)

Note: $V(-\ell) = V_0^+ e^{j\beta\ell} (1 + \Gamma_L e^{-2j\beta\ell})$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

At $\ell = d$:

$$V(-d) = V_0^+ e^{j\beta d} (1 + \Gamma_L e^{-j2\beta d}) = V_{TH} \left(\frac{Z_{in}}{Z_{in} + Z_{TH}} \right)$$

$$\Rightarrow V_0^+ = V_{TH} \left(\frac{Z_{in}}{Z_{in} + Z_{TH}} \right) e^{-j\beta d} \left(\frac{1}{1 + \Gamma_L e^{-j2\beta d}} \right)$$

Hence

$$V(-\ell) = V_{TH} \left(\frac{Z_{in}}{Z_m + Z_{TH}} \right) e^{-j\beta(d-\ell)} \left(\frac{1 + \Gamma_L e^{-j2\beta\ell}}{1 + \Gamma_L e^{-j2\beta d}} \right)$$

Example (cont.)

Some algebra: $Z_{in} = Z(-d) = Z_0 \left(\frac{1 + \Gamma_L e^{-j2\beta d}}{1 - \Gamma_L e^{-j2\beta d}} \right)$

$$\begin{aligned} \Rightarrow \frac{Z_{in}}{Z_{in} + Z_{TH}} &= \frac{Z_0 \left(\frac{1 + \Gamma_L e^{-j2\beta d}}{1 - \Gamma_L e^{-j2\beta d}} \right)}{Z_0 \left(\frac{1 + \Gamma_L e^{-j2\beta d}}{1 - \Gamma_L e^{-j2\beta d}} \right) + Z_{TH}} = \frac{Z_0 (1 + \Gamma_L e^{-j2\beta d})}{Z_0 (1 + \Gamma_L e^{-j2\beta d}) + Z_{TH} (1 - \Gamma_L e^{-j2\beta d})} \\ &= \frac{Z_0 (1 + \Gamma_L e^{-j2\beta d})}{(Z_{TH} + Z_0) + \Gamma_L e^{-j2\beta d} (Z_0 - Z_{TH})} \\ &= \left(\frac{Z_0}{Z_{TH} + Z_0} \right) \frac{(1 + \Gamma_L e^{-j2\beta d})}{1 + \Gamma_L e^{-j2\beta d} \left(\frac{Z_0 - Z_{TH}}{Z_{TH} + Z_0} \right)} \\ &= \left(\frac{Z_0}{Z_{TH} + Z_0} \right) \frac{(1 + \Gamma_L e^{-j2\beta d})}{1 - \Gamma_L e^{-j2\beta d} \left(\frac{Z_{TH} - Z_0}{Z_{TH} + Z_0} \right)} \end{aligned}$$

Example (cont.)

Hence, we have

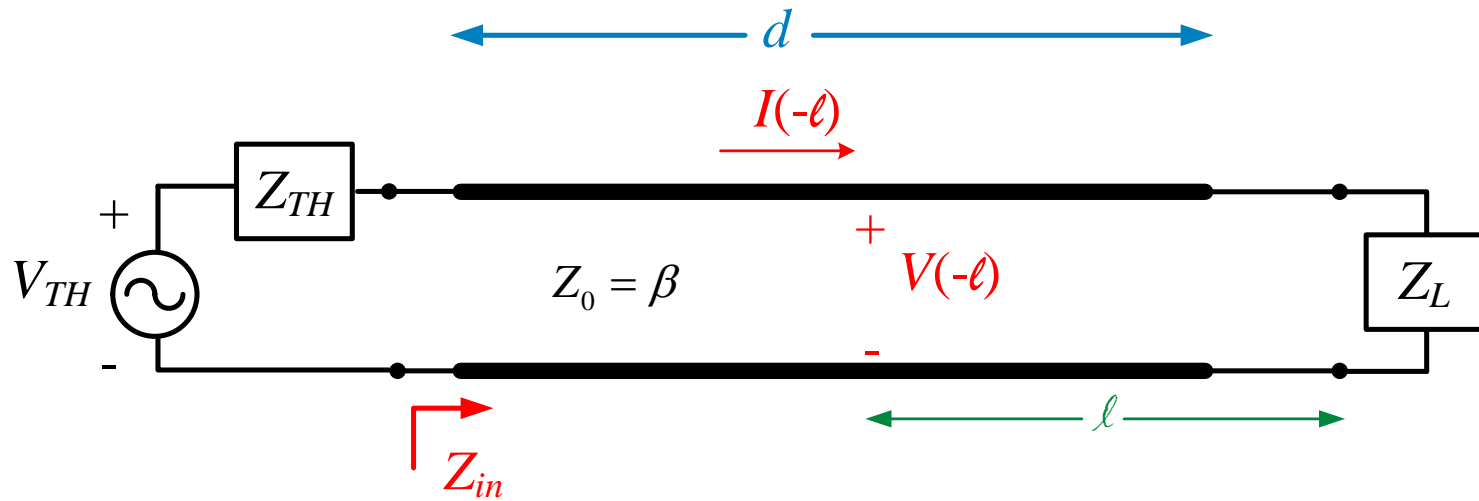
$$\frac{Z_{in}}{Z_{in} + Z_{TH}} = \left(\frac{Z_0}{Z_0 + Z_{TH}} \right) \left(\frac{1 + \Gamma_L e^{-j2\beta d}}{1 - \Gamma_S \Gamma_L e^{-j2\beta d}} \right)$$

where $\Gamma_S = \frac{Z_{TH} - Z_0}{Z_{TH} + Z_0}$

Therefore, we have the following alternative form for the result:

$$V(-\ell) = V_{TH} \left(\frac{Z_0}{Z_0 + Z_{TH}} \right) e^{-j\beta(d-\ell)} \left(\frac{1 + \Gamma_L e^{-j2\beta\ell}}{1 - \Gamma_S \Gamma_L e^{-j2\beta d}} \right)$$

Example (cont.)



$$V(-l) = V_{TH} \left(\frac{Z_0}{Z_0 + Z_{TH}} \right) e^{-j\beta(d-l)} \left(\frac{1 + \Gamma_L e^{-j2\beta l}}{1 - \Gamma_S \Gamma_L e^{-j2\beta d}} \right)$$

Voltage wave that would exist if there were no reflections ($\Gamma_L = 0$) from the load (a semi-infinite transmission line or a matched load).

Example 6

Given a 50Ω transmission line that is 0.25λ long excited by a 1V voltage source at 300MHz Frequency with an internal impedance of 100Ω , and the line is terminated by a load $Z_L = 100 - j40 \Omega$ determine $v(l = \lambda/8)$

$$V(z = -l) = V_{TH} \left(\frac{Z_0}{Z_0 + Z_{TH}} \right) e^{-j\beta(d-l)} \left(\frac{1 + \Gamma_L e^{-j2\beta l}}{1 - \Gamma_S \Gamma_L e^{-j2\beta d}} \right)$$

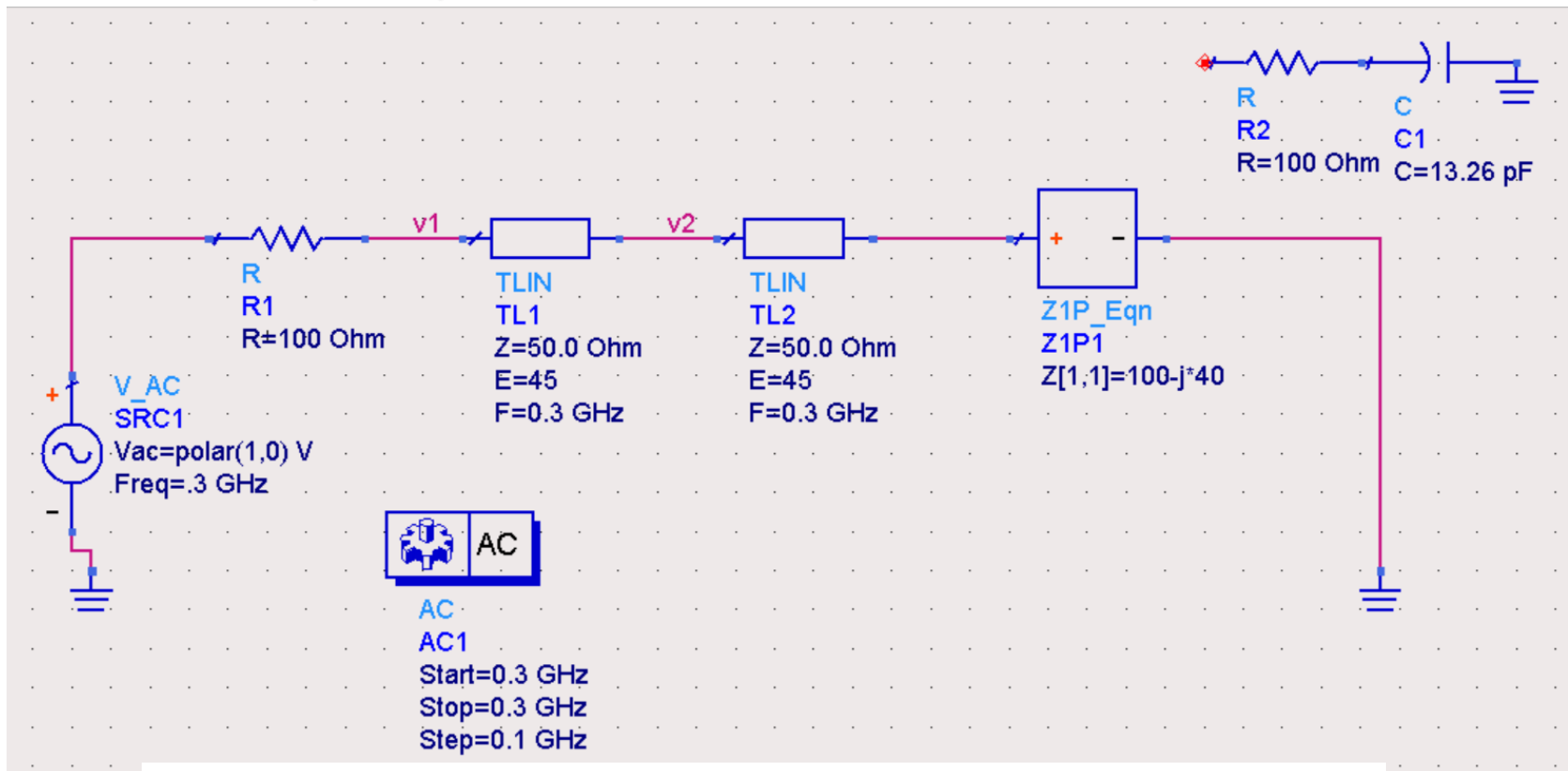
$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = 0.378 - j0.166$$

$$\Gamma_S = \frac{100 - 50}{100 + 50}$$

$$V\left(l = \frac{\lambda}{8}\right) = 1 * \left(\frac{50}{150}\right) * (e^{-j45}) \left(\frac{1 + (0.378 - j0.166)e^{-\frac{j\pi}{2}}}{1 - \frac{1}{3}(0.378 - j0.166)e^{-j\pi}}\right)$$

$$= 0.108 - j0.248$$

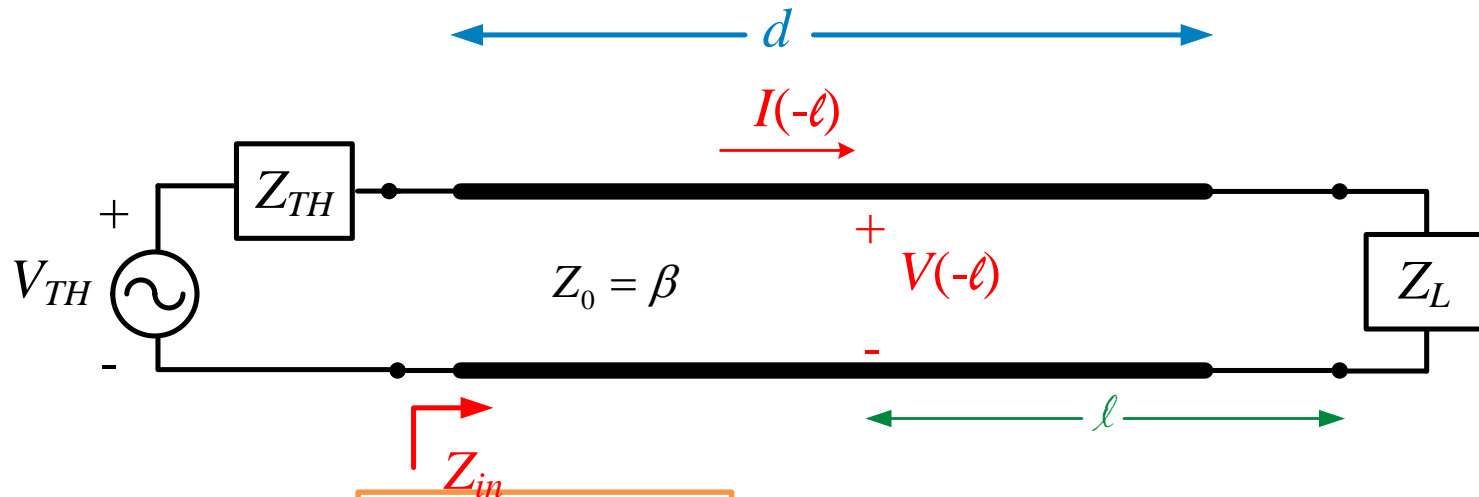
Simulate Example 6 by ADS



inputvoltage

freq	v1	v2
300.0 MHz	0.181 + j0.058	0.108 - j0.248

Special case for incident voltage when $Z_{TH}=Z_0$



$$V(-l) = V_{TH} \left(\frac{Z_0}{Z_0 + Z_{TH}} \right) e^{-j\beta(d-l)} \left(\frac{1 + \Gamma_L e^{-j2\beta l}}{1 - \Gamma_S \Gamma_L e^{-j2\beta d}} \right)$$

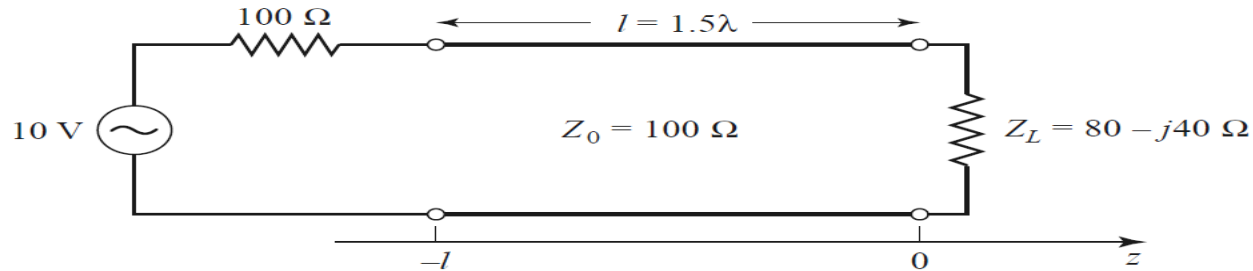
$$\Gamma_S = 0 \quad |V_0^+| = V_g / 2$$

$$\Gamma_S = \frac{Z_{TH} - Z_0}{Z_{TH} + Z_0}$$

$$Z_{TH} = V_g$$

Example 7

A generator is connected to a transmission line as shown in the accompanying figure. Find the voltage as a function of z along the transmission line. Plot the magnitude of this voltage for $-\ell \leq z \leq 0$.



$$V_0^+ = 5 \text{ V} , \Gamma_s = 0$$

$$V(-\ell) = 5 e^{-j\beta(d-\ell)} \left(1 + \Gamma_L e^{-j2\beta\ell} \right) , \quad \Gamma_L = \frac{-20 - j40}{180 - j40} = 0.24 \angle -104^\circ$$

$$l_{max} \text{ at } -104 - 2\beta l_{max} = 0$$

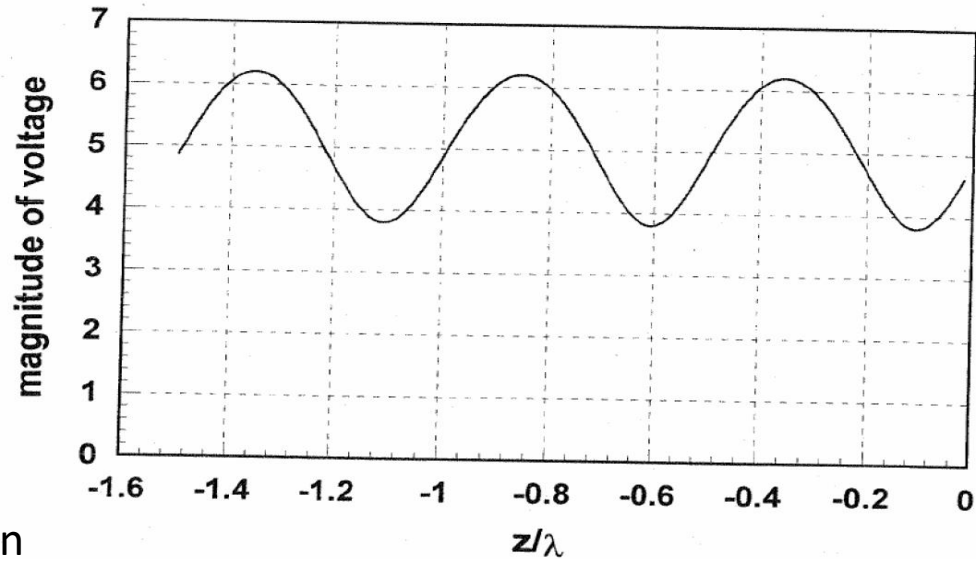
$$l_{max} = 0.355\lambda \quad \text{and} \quad V_{max} = 5(1.24) = 6.2 \text{ V}$$

$$l_{min} \text{ at } -104 - 2\beta l_{min} = \pi$$

$$l_{min} = 0.1055\lambda \quad \text{and} \quad V_{min} = 5(1 - 0.24) = 3.8 \text{ V}$$

$$l_{max} - l_{min} = \lambda / 4$$

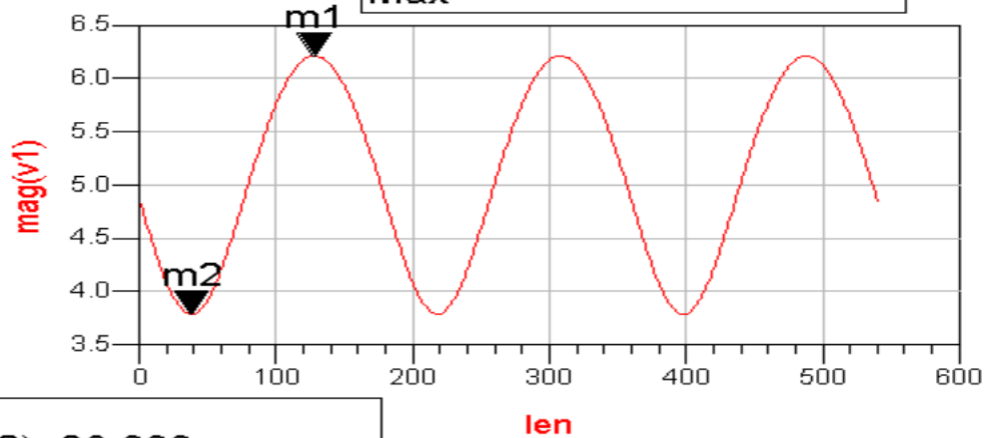
$$V_L = 10 * \frac{Z_L}{Z_L + Z_s} = 4.86 \angle -13.5^\circ$$



ADS Simulation

lmin=m1/360 lumda=0.355 lumda
lmax=m2/360 lumda=0.105 lumda

m1
indep(m1)=128.000
plot_vs(mag(v1), len)=6.213
freq=1.000000GHz
Max



m2
indep(m2)=38.000
plot_vs(mag(v1), len)=3.787
freq=1.000000GHz
Min

Voltage Standing Wave Ratio

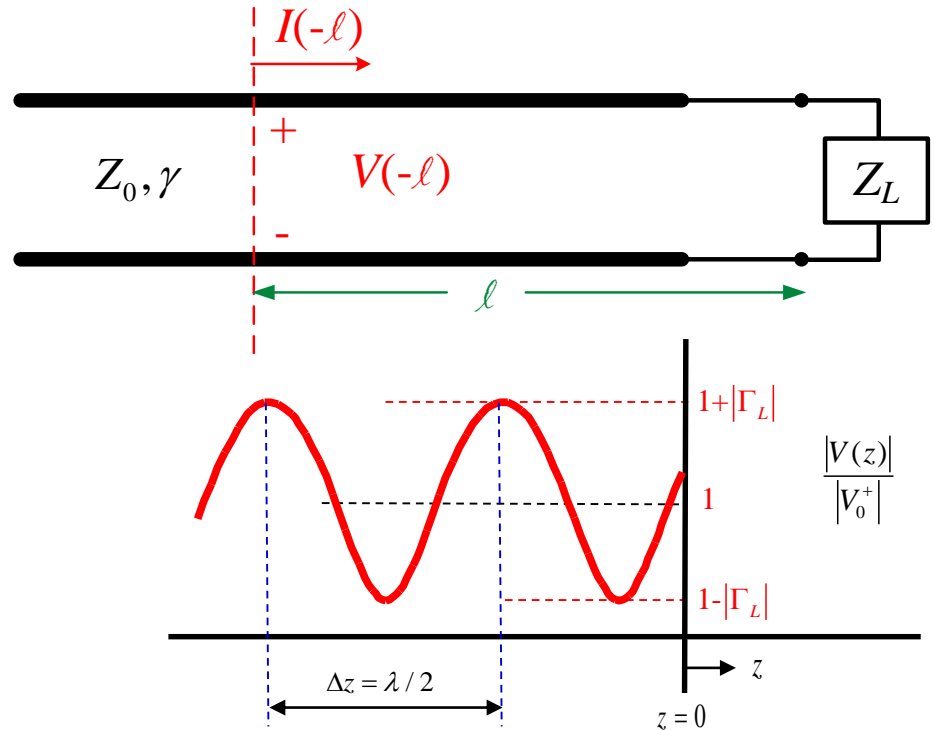
$$V(-\ell) = V_0^+ e^{j\beta\ell} (1 + \Gamma_L e^{-2j\beta\ell})$$

$$= V_0^+ e^{j\beta\ell} (1 + |\Gamma_L| e^{j\phi_L} e^{-2j\beta\ell})$$

$$|V(-\ell)| = |V_0^+| |1 + |\Gamma_L| e^{j\phi_L} e^{-j2\beta\ell}|$$

$$V_{\max} = |V_0^+| (1 + |\Gamma_L|)$$

$$V_{\min} = |V_0^+| (1 - |\Gamma_L|)$$



$$\text{Voltage Standing Wave Ratio (VSWR)} = \frac{V_{\max}}{V_{\min}}$$

$$\text{VSWR} = \frac{1 + |\Gamma_L|}{1 - |\Gamma_L|}$$